## Kufandada Irrigation Scheme: Detailed Design Report

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### Disclaimer

The British Government's Department for International Development (DFID) financed this work as part of the United Kingdom's aid programme. However, the views and recommendations contained in this report are those of the consultant, and DFID is not responsible for, or bound by the recommendations made.





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### List of Acronyms

| Acronym | Long-Form   |  |
|---------|---|--|
| ASI     | Adam Smith International                                    |  |
| AC      | Asbestos Cement   |  |
| BADEA   | Arab Bank for Economic Development                          |  |
| AGRITEX | Department of Agricultural Technical and Extension Services |  |
| СВА     | Cost Benefit Analysis                                       |  |
| CBMP    | Community Based Water Management Project                    |  |
| CRIDF   | Climate Resilient Infrastructure Development Facility       |  |
| DDF     | District Development Fund                                   |  |
| DFID    | Department of International Development                     |  |
| ENPV    | Economic Net Present Value                                  |  |
| EOCC    | Economic Opportunity Cost of Capital                        |  |
| FOCC    | Financial Opportunity Cost of Capital                       |  |
| ERR     | Economic Rate of Return                                     |  |
| ECC     | Engineering Construction Contract                           |  |
| EIA     | Environmental Impact Assessment                             |  |
| EMA     | Environmental Management Agency (Zimbabwe)                  |  |
| EMP     | Environmental Management Plan                               |  |
| FAO     | Food and Agricultural Organisation                          |  |
| FBCR    | Financial Benefit-Cost Ratio                                |  |
| FIRR    | Financial Internal Rate of Return                           |  |
| FNPV    | Financial Net Present Value                                 |  |
| GRP     | Glass Reinforced Plastic                                    |  |
| ICZ     | Interconsult Zimbabwe (Pvt) Itd                             |  |
| MC      | Management Contract(or)                                     |  |
| MDPE    | Medium Density Polyethylene                                 |  |
| MFI     | Micro-Finance Institution                                   |  |
| MSMEC   | medium scale enterprises and cooperatives                   |  |
| NGO     | Non-Governmental Organisation                               |  |
| O & M   | Operation and Maintenance                                   |  |
| P and G | Preliminary and General                                     |  |
| SADC    | Southern Africa Development Community                       |  |
| SSA     | Sub-Saharan Africa  |  |
| TOR     | Terms of Reference  |  |
| USD     | United States Dollar  |  |



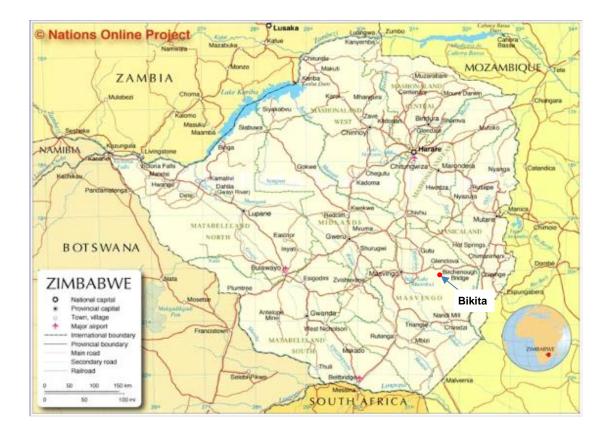
| VIP Latrine | Ventilated Improved Pit Latrine      |
|-------------|--------------------------------------|
| WASH        | Water Supply, Sanitation and Hygiene |
| ZINWA       | Zimbabwe National Water Authority    |
| ZIMVAC      | Zimbabwe Vulnerability Assessment    |

### **Executive Summary**

### Background

The proposed Kufandada Irrigation is among a number of Quick Win water projects identified for possible development in the region under CRIDF to be delivered relatively quickly in order to demonstrate immediate benefits. Following reconnaissance and feasibility studies, the project was selected for support under the Facility.

The proposed Kufandada irrigation scheme will benefit three villages of Ndimo, Nhamo, and Mandivengerei Villages in Wards 10 and 13 of Bikita District with an estimated 120 households. The location of the scheme is shown in the map below.



Following a reconnaissance visit to the project area, and assessment for possible support, the project was screened and found to comply with CRIDF's requirements. A decision was then made to provide support for the feasibility assessment of the project. This was undertaken and completed during the last quarter of 2014. The feasibility study developed technical aspects of the project through optioneering, and cost-benefit analysis, which established the financial and economic viability of the project. Further screening resulted in a decision to provide support for the implementation of the project. This report is an outline of the key technical components of the project, the manner in which they will be implemented, as well as Bill of Quantities and Cost Estimates.

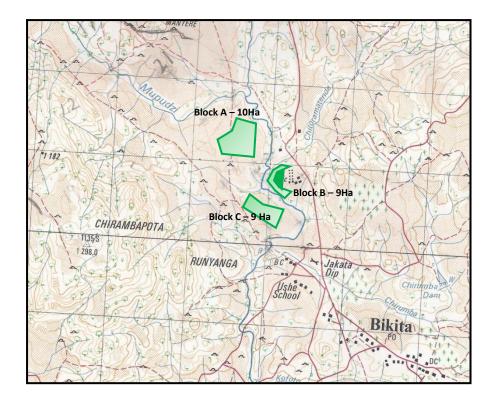


### **Project Description**

The project area is wholly located in communal land where the community mainly depends on rain-fed agriculture production to meet its food requirements, and rainfall patterns are no longer predictable as they were in the past. The main elements of the project are the irrigation scheme, water supply and sanitation as well as river and environmental protection.

### Proposed Irrigation Scheme

Local traditional and community leaders have identified 28 ha of land distributed among three blocks to be incorporated in the irrigation scheme. The location of the irrigation blocks is shown below.



The land is currently being utilised under rain-fed farming. It is owned by individual households, who have ceded their land for common use under the proposed scheme. The scheme also includes land which has been provided by the Bikita Hospital to establish a nutrition Garden for patients as well as staff.

Analysis of rainfall data from a nearby rainfall stations shows a decreasing rainfall trend after 1999/2000 to 2013/14.

It is proposed to utilise yield from the perennial Mupudzi River as a source of water for the irrigation scheme. The supply from the river will be supplemented by releases from the upstream Rozva dam. ZINWA has given an undertaking to issue an abstraction permit and to enter into a memorandum of agreement for the supply of additional water from the dam, if required during low flows.



Hydrological analysis indicated that 28 ha could be irrigated from the average yield of the combined flow from Mupudzi River and Chitoramatende River, supplemented by releases from Rozva dam during periods of low flow. The irrigated area is apportioned between the three irrigation blocks as follows:

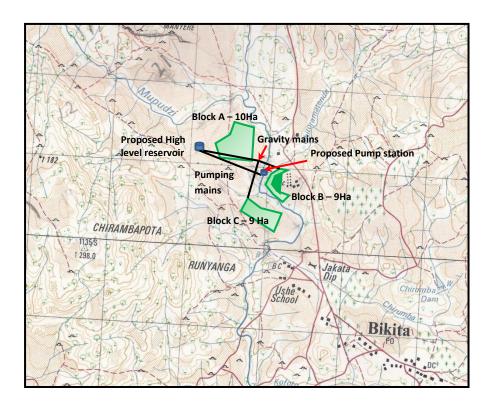
Block A - 10 ha

Block B - 9 ha

Block C - 9 ha

The adopted design criterion for the bulk water supply for irrigation is based on the delivery of water to night storage over a maximum period of 16 hours using the industry standard which assumes a water demand of 15,000 m3/ha/annum. This results in a design flow of 157.3 m<sup>3</sup>/hr for the pumping system. With respect to infield irrigation, the FAO approach has been adopted which gave a design flow of 204.6 m<sup>3</sup>/hr for the delivery to the field.

It is proposed to abstract water from Rozva River at a location approximately 250m downstream of existing Kufandada Dam for the irrigation scheme. The general layout of the scheme is shown in schematic below.



Water will be pumped from the river to night storage reservoirs located at an elevated location west of the river. From the night storage reservoirs, it will gravitate to the irrigation fields.

#### Water supply and sanitation

Options for the water supply were investigated, including connection to the ZINWA system and the provision of groundwater supplies. It is recommended that two new boreholes be drilled, as well as the rehabilitation of



the broken down hand pump at the existing borehole. The proposed delivery mode for sanitation is for the project to supply selected building materials for 24 VIPs with the beneficiaries providing construction labour.

### **Environmental protection**

There is widespread stream bank and in-stream cultivation along the Rozva River and its tributaries. This has resulted in extensive water habitats destruction and siltation of water bodies. It is proposed to re-establish the statutory 30m buffer protection zones and plant grass and indigenous trees for protection in select areas.

### Cost Estimates and Bill of Quantities

Bill of Quantities have been developed based on abstraction of water from Rozva River and the irrigation of 28 ha, including the provision of 2 new boreholes, the rehabilitation of a one, and supply of building materials for the construction of VIP latrines. It is estimated that the project will cost USD



### Introduction

### Background

The Climate Resilient Infrastructure Development Facility (CRIDF), supported by DFID aims to deliver sustainable small-scale infrastructure across 11 SADC countries. The demand driven programme focuses on water services, water resources management and agriculture with the objective of creating a lasting impact on the region's water and food security. Among a number of parallel programmes, CRIDF will support projects which can be delivered relatively quickly, to demonstrate immediate benefits. To this end, the CRIDF team has carried out high level consultations to identify these "Quick Win" projects throughout the region.

The feasibility study for the proposed river protection irrigation scheme established that the environmental protection works and irrigation of approximately 28 ha of land from a new take-off weir on Rozva River at Kufandada village near Bikita, Zimbabwe, was technically feasible. It also demonstrated the financial and economic feasibility of the project, and that there were significant positive environmental impacts arising from its implementation. This report outlines the development of a technical design for the Kufandada Irrigation Scheme based on the option selected at feasibility stage. It covers salient technical issues to provide the back ground of key components of the project to enable its construction.

The proposed Kufandada irrigation scheme will benefit three villages of Ndimo, Nhamo, and Mandivengerei Villages in Wards 10 and 13 of the District with an estimated 120 households. In addition, the scheme will also benefit the Bikita Rural Hospital and its staff.

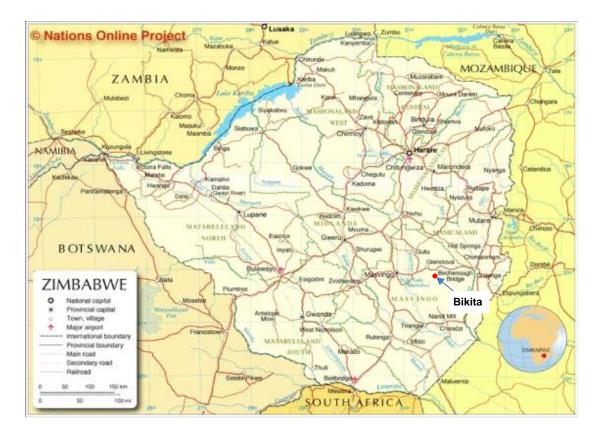
### Project Location and Site Access

The proposed project area is within three villages called Ndimo, Nhamo and Mandivengerei Villages which are in wards 10 and 13 of Bikita District. All these villages are located approx. 7km from Nyika Growth Point and 3km from Bikita DA's offices which is the local government service centre for the district. Figure 1 bewlow shows the location of Bikita District Administrative Centre.

Access to the proposed scheme is via the main road from Nyika Growth Point, which branches off the Masvingo road to turn southwards to Bikita District Centre. The scheme is located across the Rozva River just south of Bikita Hospital.

The villagers are mainly peasant farmers with a few of them employed by local government agencies and other private enterprises at Bikita Service Centre and Nyika Growth point respectively. There are no major economic activities in the area except some commercial farming activities at nearby Rozva dam located near Nyika Growth Point and also other dams located further south of Bikita. Bikita Minerals, a world renowned lithium producer is some 30km away.

### Figure 1 Location Map



The project area is located in relatively dry agro-ecological region III of Zimbabwe where yearly rainfall typically ranges from 650 to 800mm. The soils in the area are generally sandy gravelly loam soils and the peasants there are mostly involved in seasonal cultivation of the staple crop maize.

### Structure of the Design Report

This report covers salient technical aspects on the design of Kufandada Scheme to provide some context to the accompanying design drawings. It covers a general description of the project area, the main components of the scheme, design assumptions and key hydraulic features, concerning the transfer of water from proposed river abstraction works to the irrigation fields.



### **Project Description**

### General Description of the Project Area

The project area is wholly located in communal land where the community mainly depends on rain-fed agriculture production to meet its food requirements. However, the rainfall pattern is no longer as predictable as it was in the past, with the now frequent short rainfall season resulting in poor agricultural yields. Most farmers have adopted conservation agriculture in an effort to increase crop yields while contour ridging is no longer common. Although there is still a dependence on livestock, the number of large livestock has dwindled significantly. Most poor households derive their livelihoods from the sale of wild fruits (mashuku and chakata), while the able bodied community members depend on casual work at the nearby business centres and the fledgling Rozva and Shereni irrigation schemes, 7 and 30km away respectively.

There is rapid urbanization affecting the two wards due to the nearby Bikita administrative centre, where parts of ward 13 have now been co-opted in the centre's development plans.

Water supply coverage is generally poor although some villagers have private connections from the ZINWA system which supplies Bikita. Generally the villagers get water for their domestic purposes in shallow and deep wells. Of three boreholes constructed and equipped with bush pumps only one is still functional. Consequently, some villagers walk more than a kilometre to the existing borehole to augment their domestic water supplies

Land-use is dominated by rain-fed agriculture, grazing and small gardens. Due to the hilly terrain, isolated patches of vegetation flourish on the slopes which used to provide a habitat for large forms of wildlife such as hyenas, baboons, kudu, buck, rock rabbits and hares. In general wild life population has declined due to habitat destruction and unrestricted hunting in the area. Grasslands occur on the edges of crop fields and provide pastures for the cattle.

The Mpudzi River as well as the Rozva River transport large volumes of silt that is washed into the river from the hinterland. This resulted in the silting of the Kufandada Dam, which was constructed some 20 years ago. Water passes over the silted weir, and is used by community members for laundry, bathing and livestock watering

Key environmental issues in the project area are land degradation, climate change, declining water availability and siltation of the streams, exacerbated by general poverty and over-dependence on natural resources for livelihoods. Unsustainable land management practices are aggravated by periodic droughts and floods. The Save River Basin has become so heavily degraded that the Environmental Management Agency has declared it a basin requiring 'restoration'.

The primary energy source for cooking in ward 10 and 13 is firewood, with very few people connected to the nearby electricity grid. The project area was selected for CRIDF support because of its vulnerability to

climate change, poor land use practices that impact negatively on transboundary water resources, the prevalence of extreme poverty, a high rate of population increase, frequent natural disasters such as droughts



and floods, and agricultural systems (both crop and livestock production) that depend heavily on rainfall. Climate variability and change have further exacerbated the scarcity of natural resources such as forests, with the consequent loss in the biodiversity of flora and fauna. Predictions for the Bikita area indicate that changes in temperature and weather patterns were affecting the frequency and severity of rainfall, droughts, floods, access to water and the use of land.

### Available Irrigation land and soil suitability

Local traditional and community leaders have identified three blocks of land to be incorporated in the irrigation scheme. The location of the irrigation blocks is shown in Figure 1 below.

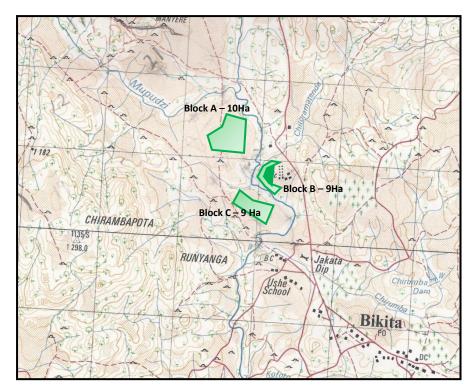


Figure 2 Location of identified irrigation land

The land is currently being utilised under rain-fed farming. It is owned by individual households, who have ceded their land for common use under the proposed scheme. The scheme also includes land which has been provided by the Bikita Hospital to establish a nutrition Garden for patients as well as staff.

A preliminary visual assessment that was undertaken during a recent site visit indicated similar soil types for all the tree blocks, dominated by sandy soils overlaying a soft quartzite rock. Terrain is gently undulating (3-5% slope) with visible signs of soil erosion including rills. Reworking of the soils is proposed to improve the soil for irrigation. This includes deep ploughing, accompanied initially by high rates of application of fertiliser and irrigation water.

### Summary of the Hydrology



### General climate

The hinterland area falls within agro-ecological region 4. However, the area around the project area has a micro- climate where rainfall is generally higher than the rest of the region. Consequently, it been classified under Region 3. Mean annual temperature is below 20<sup>°</sup> centigrade, while mean maximum temperatures are around are 30<sup>°</sup> centigrade. Long term mean annual rainfall is in excess of 1,000 mm. Analysis of rainfall data from a nearby rainfall stations shows a decreasing rainfall trend after 1999/2000 to 2013/14.

#### Existing Sources of Water

It is proposed to utilise yield from the perennial Mupudzi River as a source of water for the irrigation scheme. The river drains an area where rainfall is in the region of 1000 mm per annum. It enters Rozva River just above the Kufandada dam. A minor tributary, the Chitoramatende flows into Rozva River just below the dam. Yield analysis was undertaken at a location on Mupudzi River above the confluence with Rozva River, and below Kufandada dam after the confluence of Rozva River with Chitoramatende River. The results are summarised below:

| Above the confluence with Rozva River |                                  |  |  |  |
|---------------------------------------|----------------------------------|--|--|--|
| 10% yield                             | 186,400 m <sup>3</sup> per annum |  |  |  |
| 20% yield                             | 286,386 m <sup>3</sup> per an    |  |  |  |

| Just below the confluence Chitoramatenda |                                  |  |  |  |  |
|--|----------------------------------|--|--|--|--|
| 10% yield                                | 225,544 m <sup>3</sup> per annum |  |  |  |  |
| 20% yield                                | 346,528 m <sup>3</sup> per annum |  |  |  |  |

The 20% yield of 346,528 m<sup>3</sup> per annum is adequate to meet the water demand for the 28 Ha irrigable lands. However, government policy requires the use of 10% yield for the planning of irrigation schemes.

#### Water rights and permits

A permit will be required from the Catchment Council to abstract water from Rozva River utilising the yield from Mupudzi River. There will also be a need to enter into a Memorandum of Agreement with ZINWA to obtain water from Rozva dam to supplement supplies in the event of low flows. ZINWA has given an undertaking that the permit will be made available, including entering into a Memorandum of Agreement to facilitate access to water from Rozva Dam for the irrigation scheme.

### Water demand



#### Irrigation water demand

The estimation of irrigation water demand has been based on industry accepted standards for the region. The results of the analysis have been used in the design of the bulk water supply, as well as the sizing of irrigation land to be developed.

**Error! Reference source not found.** below gives indicative values of water requirements for common cereal and horticultural crops in Zimbabwe

| Crop      | Water need (mm/total | Sensitivity to drought |
|-----------|----------------------|------------------------|
|           | growing period)      |                        |
| Bean      | 300-500              | Medium-High            |
| Cabbage   | 350-500              | Medium-High            |
| Maize     | 500-800              | Medium-High            |
| Onion     | 350-550              | Medium-High            |
| Groundnut | 500-700              | Low-Medium             |
| Potato    | 500-700              | High                   |
| Soya bean | 450-700              | Low-medium             |
| Tomato    | 400-800              | Medium-High            |

#### Table 1 Indicative values of crop water needs and sensitivity to water shortage

The analysis of bulk irrigation water demand was based on the following assumptions derived for the irrigation of 28 ha. It does not take into account the varying crop water requirements for different crops or efficiencies that can be realised by the various irrigation methods in common use. It has been used in the sizing of bulk water delivery components and to develop the general layout of infield irrigation systems.

| Duration of irrigation cycle*   | : | 7 days                    |
|---|---|---------------------------|
| Irrigation days per cycle   | : | 5 days                    |
| Rate of application   | : | 45 mm per ha/ application |
| Total available irrigable land  | : | 28 ha                     |
| Total irrigation period per year (April – Nov)  | : | 244 days                  |
| Total no of cycles per year = 244/7   | : | 34.85                     |
| Therefore Irrigation water demand per ha/ year( $45 \times 10^4 \times 34.85$ )/ $10^3 \text{ m}^3$ | : | 15,682 m <sup>3</sup>     |
| Effective irrigation days per year = 5 x 34.85  | : | 174.28 days               |
| Total area of irrigation fields   |   | 28 ha                     |

| Total annual water demand for ha                                 | : | 439,096 m <sup>3</sup>    |
|--|---|---------------------------|
| Nominal area to be irrigated per cycle                           |   | 5.6 ha                    |
| Total water demand per day                                       | : | 2,520 m <sup>3</sup>      |
| 10% Yield of Mupudzi at the confluence with Chitoramatende River | : | 1,294 m <sup>3</sup> /day |

The above indicates a shortfall of 1,226 m<sup>3</sup>/day, at a 10% level of service. The average yield of Mupudzi River is estimated at 5,312 m<sup>3</sup>/day. Thus on average, there will be adequate flow to cater for the planned irrigation scheme, with shortfalls being experienced during periods of low flow. As indicated earlier, these shortfalls will be supplemented by releases obtained from Rozva Dam.

### Domestic water demand and sanitation coverage

Villagers get water for their domestic purposes from shallow and deep wells. During good rainfall years water is generally available for domestic purposes. However there are reports that shortages occurred in the past and some boreholes were sunk by some non-governmental organisations to assist the villagers.

Of three boreholes constructed and equipped with bush pumps only one is still functional. Some villagers walk more than a kilometre to the existing borehole to augment their domestic water supplies.

| Estimated No. of households                    | 120             |
|--|-----------------|
| Assuming a household size of                   | 4.5             |
| Total estimated population in the project area | 540             |
| Unit water consumption                         | 20 l/person/day |
| Total water demand per day                     | 10.8 m3         |

Existing water supplies consist of one functional borehole in Nhamo Village, and two which have broken down hand pumps. One site was surveyed but not drilled.

#### Livestock water consumption

Because of relative good availability of perennial river flows on Rozva and Mpudzi Rivers, water for domestic animal consumption is considered to be adequate.

### Description of Kufandada Irrigation Scheme

#### Size of irrigation scheme

Hydrological analysis indicated that a total of 28 ha could be irrigated from the average yield of the combined flow from Mupudzi River and Chitoramatende River supplemented by releases from Rozva dam during periods of low flow. The irrigated area is apportioned between the three irrigation blocks as follows:

Block A - 10 ha

Block B - 9 ha

### Block C - 9 ha



Two sites have been investigated for the abstraction of water to irrigate the above blocks. The locations of the sites are shown in the excerpt from the 1:50,000 map Figure 3 below.

### Site 1 – Weir on Mupudzi River

Site 1 is located on Mupudzi River, approximately 300 m upstream of the confluence with Rozva River, at geographic co-ordinates 20° 3.45'S and 31° 35.93'E. There are no rock outcrops visible at the site, which would be suitable for the 5 m high, 130 m long earth dam. The purpose of the dam will be to facilitate the diversion of water to the pump station located on the left bank. It would be a run-off river arrangement with minimum storage, receiving flows only from the Mpudzi River.

The riverbed elevation is approximately 926 m above mean sea level. Assuming a total freeboard of 3 m the dam would raise the water level to a minimum of 929 m.

#### Site 2 – Weir on Rozva River

Site 2 is located on Rozva River, approximately 240 m downstream of the existing Kufandada Dam, at geographic reference 20° 3.958'S and 31° 36.193'E, just after the confluence with Chitoramatende River. The site has solid rock outcrops across the width of the river channel, which offers ideal foundation conditions for a masonry weir. The pump station would be located on the right bank.

The weir will act as a pick-up facility to facilitate abstraction of water from the Rozva River. It will receive flows from both Mupudzi River and Chitoramatende River, both tributaries of the Rozva River. It will also be possible to utilise releases from Rozva Dam during periods of low/no flows in the Mupudzi and Chitoramatende Rivers.

### <u>CRID</u>F

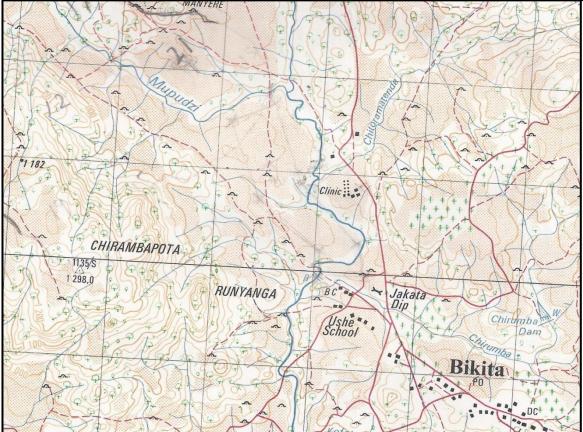


Figure 3 Locations of potential abstraction sites

The riverbed elevation is approximately 910 m above mean sea level. Assuming a weir height of 3 m, the weir will raise the water level to a minimum of about 913 m.

A comparative analysis of the two sites was undertaken at feasibility stage and Site 2 selected for the diversion of water to the irrigation blocks.

### Design flows

### Bulk water Supply to Night Storage

The adopted design criterion for the bulk water supply is based on the delivery of bulk water to night storage over a maximum period of 16 hours using the industry standard which assumes a water demand of 15,000 m<sup>3</sup>/ha/annum.

The calculated design flows for the irrigation of 28 ha of Block A are as follows:

Delivery to night storage -  $0.044 \text{ m}^3/\text{s} = 157.5 \text{ m}^3/\text{hr}$ 

The above flow was used to design the pumping mains for the delivery of bulk water supply.



### Irrigation Water Demand at the Field

Irrigation water demand depends on the type of soils, climate, topography and the irrigation system employed. The selection of the most appropriate irrigation system was based on agro-socio-economic characteristics of the commonly used irrigation systems in Zimbabwe. The drag line sprinkler irrigation system was selected as the most suitable one for adoption at Kufandada Irrigation Scheme.

The FAO approach was adopted to determine the irrigation demand at the field based on sprinkler irrigation of a maize crop. The results are summarised in Table 2 below.

| Area to be irrigated (ha)               | 28         |                        |
|---|------------|------------------------|
| Pan evaporation rate (mm/day)           | 8          | Bindagombe Dam Station |
| Crop factor (f)                         | 0.7        |                        |
| Water holding capacity (mm/m)           | 55         | Sandy loam             |
| Infiltration rate of the soil           | 12         |                        |
| Effective rooting depth(m)              | 0.9        |                        |
| % allowable water depletion             | 50         |                        |
| System efficiency (%)                   | 80         |                        |
| Effective rainfall (mm/day)             | 0          |                        |
| lateral spacing (m)                     | 18         |                        |
| Sprinkler spacing (m)                   | 12         |                        |
|   |            |                        |
| Calculated                              |            |                        |
| Evapotranspiration(mm/day)              | 5.6        |                        |
| Readily available water(mm)             | 24.8       |                        |
| Net irrigation requirement (mm/day)     | 5.6        |                        |
| Gross irrigation requirement (mm/day)   | 7          |                        |
| Calculated Cycle Length                 | 4.4        |                        |
| Actual Cycle Length                     | 5          |                        |
| Irrigable land per day (Ha)             | 5.6        |                        |
| Wetted area (m <sup>2</sup> )           | 216        |                        |
| Application rate (mm/h)                 | 7.87       |                        |
| Sprinkler discharge (m <sup>3</sup> /h) | 1.7        |                        |
| Gross application rate (mm/h)           | 7.87037037 | Sprinkler size is ok   |

#### Table 2Irrigation design data based on a maize crop

| Net application rate (mm/hr)                   | 6.3   |     |
|--|-------|-----|
| standing time (hr)                             | 3.9   |     |
| No of sets per day                             | 2     |     |
| Working hours per day (hr)                     | 7.9   |     |
| No of sets per cycle                           | 10.0  |     |
| Gross application per cycle (mm)               | 35.0  |     |
| No of sprinklers operating simultaneously( >=) | 130   |     |
| System Capacity (m <sup>3</sup> /hr)           | 220.4 |     |
|  |       |     |
|  | 61.2  | l/s |

The above design flows were used to size the pumping system and gravity mains.

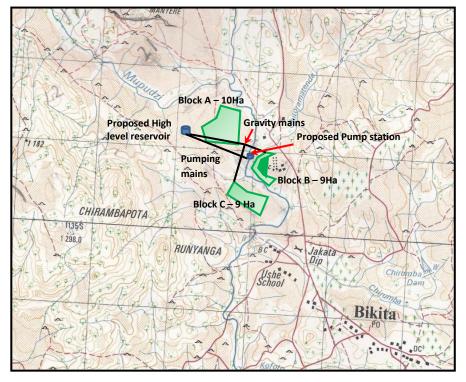
#### **General layout**

It is proposed to abstract water from Rozva River at a location approximately 250m downstream of existing Kufandada Dam to irrigate 28 ha of land distributed in the three blocks as described above. The general layout of the scheme is shown in schematic Figure 4 below. Water will be pumped from the river to night storage reservoirs located at an elevated location west of the river. From the night storage reservoirs, it will gravitate to the irrigation fields. A description of the key components of the scheme is outlined in the following sub-sections.

#### Pick-up Weir on the Rozva River

It is proposed to construct a masonry gravity pick-up weir on Rozva River just downstream of the confluence with Chituramatenda River. The selected site of the weir is rocky, with numerous boulders. A photograph of the site is shown in Figure 5 below. Foundation conditions are expected to be adequate to support the masonry structure. However, conditions in the right bank are uncertain due to the absence of a visible rock outcrop. The weir will be 40 m long and 3.5 m high, at the deepest section of the river. The crest of the weir will be 1 m wide with a downstream of 4:3, and a vertical upstream face. The stability of the weir was checked against overturning, sliding and uplifting at a maximum flood surcharge of 2.5 m above the crest using CADAM 2000 software and found to be adequate. The output from the stability computations is presented in Appendix 1.

The intake will comprise a raised bellmouth pipe in a screened chamber connected to a 40 m long, 300mm diameter suction pipe leading to the pumping station in the right bank, downstream of the weir. A gate valve on the suction main and within the pumping station is proposed for maintenance and installation of additional appurtenances.





Depending on ground conditions in the right bank of the river established during the start of construction, it is proposed to protect the right weir abutment with a combination of gabions, rock and stone pitching. A barrier to deliberately block access to the top of the weir to discourage villagers and kids will be installed

The weir has been design as a run-of-river structure primarily to raise the water level, with minimal upstream storage.

### Suction Main

The suction main is a 40m long 300mm diameter steel pipe which terminates in a 400mm diameter suction manifold pipe within the pumping station. An isolation gate valves to allow repairs is proposed within the pumping station. At the inlet point, the suction pipe will be fitted with a gate to isolate the pump station during maintenance.

Thrust blocks have been designed to provide support on all the bends along the pipeline. Concrete encasement has also been designed where there is little cover.



Figure 5 Pick-up weir site

#### **Pump Station**

The pump station will be located downstream of the weir, above flood level. It will be an excavated dry pit on the right bank. Two centrifugal pumps will be provided, one duty with one standby pumping, delivering 158 m<sup>3</sup>/hr against a total head 60 m. The pumps are designed to switch on and off when the reservoirs are full by use of a level switch. The pumps will be driven by a 32 kW, 3-phase, 4-pole electric motors supplied from a dedicated ZETDC transformer.

The low level dry pit of the pump station will ensure a flooded suction under all operating conditions.

The 10 m long and 6 m wide pump station building will be constructed from brick under corrugated iron / fibreglass roof sheeting, supported on steel trusses. A 1.5 tonne overhead crane will be provided to facilitate installation and maintenance.

Inlet and outlet pipework has been designed with 45° bends to limit head losses in the pump station, particularly on the suction side.

There will be provision for pump attendants quarters, designed to ZINWA standard. The installation will be fenced and gated to provide security.

### **Pumping Mains**

From the pump station water will be delivered to 2 No 1 MI prefabricated night storage reservoirs located on a hill through an 950m long, 200 mm diameter, mPVC Class 16/Steel pipeline. Air and scour valves will be provided as necessary along the pipeline.

Thrust blocks have been designed to provide support on all the bends along the pipeline.

#### Night Storage



Two prefabricated night storage reservoirs each with a capacity of 1 ML will be supported on reinforced concrete floor slabs at the top of the knoll. The reservoirs will be fabricated from high yield galvanised iron sheeting, and lined internally with 1 mm thick PVC.

A valved bifurcation will supply both reservoirs simultaneously from the pump station. There will be separate outlets from the reservoirs, which will lead to a second bifurcation to deliver water from both reservoirs simultaneously into the gravity mains.

#### **Gravity Mains**

Water will gravitate from the storage reservoir through a 773 m long 250 mm diameter Class 6 mPVC pipeline which passes through the middle of block A in the east, feeding into secondary mains that supply the block. At the end of the block, on its eastern boundary, the pipeline will turn southwards, reducing in diameter to 200 mm class 6 mPVC piping, and running for 309 m before bifurcating near the pump station to feed Block B to the east and Block C in the south. The 390 m long limb supplying block B will cross the river just below the weir, passing through a grave yard, to terminate at the western boundary of the block. The section across the river and through the graveyard will be laid over the 95 m span in steel piping. From the bifurcation, block C will be fed by a 478 m long 200 mm diameter mPVC class 6 buried pipeline except at stream crossings where steel, supported on concrete columns, will be used.

Air and scour valves will be provided as necessary along the pipeline. Thrust blocks have been designed to provide support on all the bends along the pipeline.

#### Infield Irrigation Systems

Analysis of the three different irrigation systems selected the drag hose sprinkler irrigation system as the most suitable for adoption for Kufandada irrigation scheme. It is adaptable to any terrain, as well as small irregular plots. In addition, nearly all crops can be irrigated by the system, although the characteristics of the crop, especially the height, have been considered in system selection.

A preliminary design of the system has been undertaken to establish the general lay out of the systems. Final design will be carried out by the equipment supplier.

Typical design data for the system based a maize crop and the size and geometry of the irrigation field is summarised in Table 2 above.

### System Hydraulics

### Pumping systems

Figure 6 below shows the hydraulic grade line for the suction and pumping mains. Suction conditions are flooded throughout the pipeline, with all pressures in the pumping main are above the allowable maximum working pressure. The contractor will be required to make the final pump selection which will need to be



approved by the Engineer. The final control philosophy of the pumps will also be jointly developed with the contractor to suit final selected pump.

A preliminary pump selection was carried out based on a KSB pump series. The most suitable pump was found to be the Etanorm 100-08-250. The pump performance and system curves are shown in Figure 7 below. Conditions in the pumping main will be as follows:

Manometric discharge head at normal operating level (weir crest level) = m

Suction conditions for the pump considered are as follows:

Available NPSH = 9.5 m

Required NPSH = 4 m

While the design has been made on the KSB model to test functionality, the BoQs will refer to pump duty point requirements, and not specific pump model.

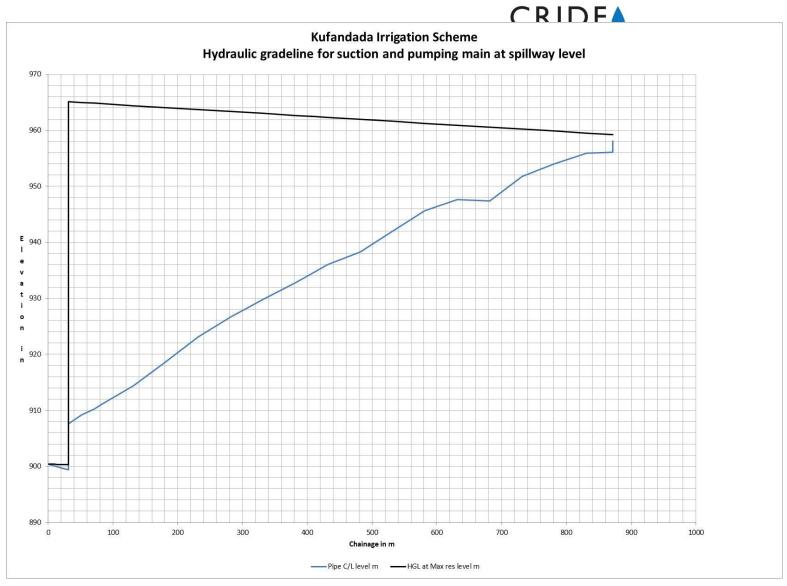


Figure 6 Hydraulic gradeline for suction and pumping mains

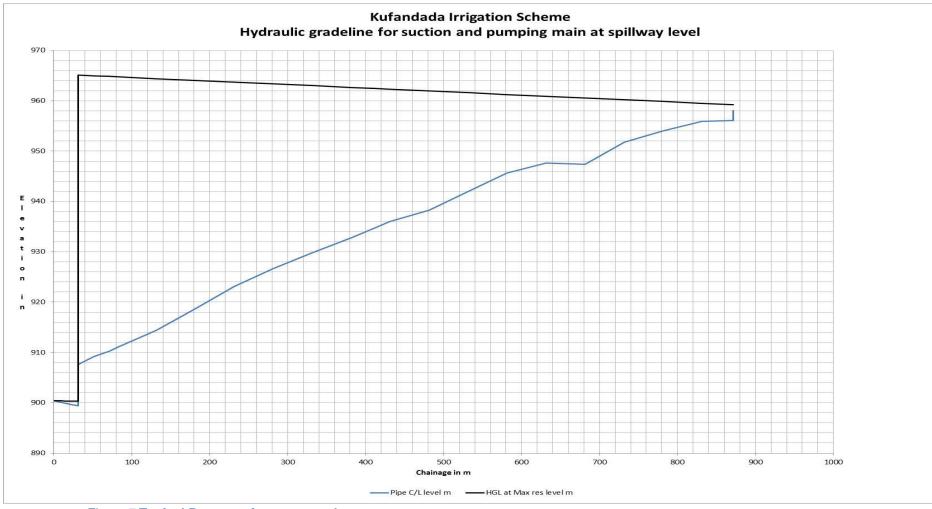


Figure 7 Typical Pump performance and system curve



#### **Gravity Mains**

The gravity mains has been designed to ensure adequate pressure in the in-field irrigation system, in as far as is possible, within the constraints of the existing topography. Pressures in Block A range from about 14.05 at the upstream end of the secondary main, increasing to about 39 m at the extreme end to the east of the block. The lower pressures in the western side are due to the higher elevations in the western portion of the block. *It will be necessary to use hose pipes for irrigation in the low pressure zones when demand in the system is close to maximum and pressures are low.* All areas under Block B and C are within the minimum design pressure zone of around 30 m for the use of sprinkler irrigation.

Rapid valve closure at the delivery to the irrigation field within a period of less than critical time of 2.5 seconds will result in maximum surge pressures being experienced in the system.

Day 1, 12:00 AM

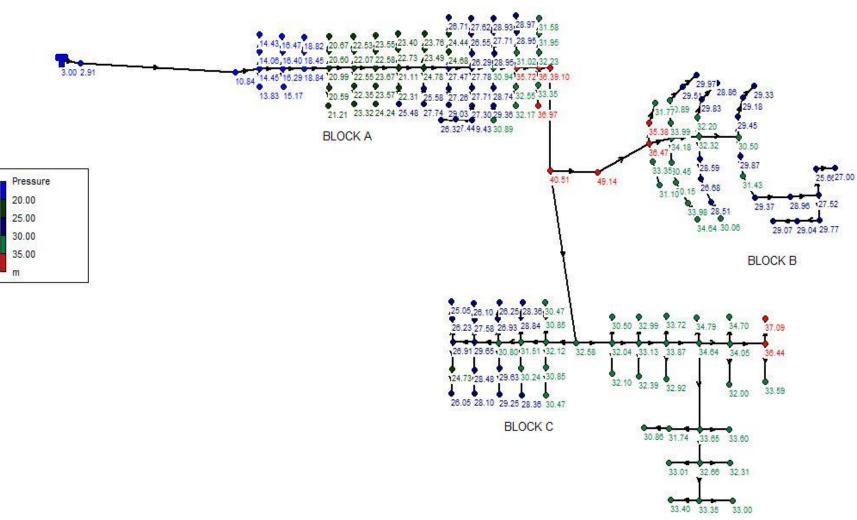
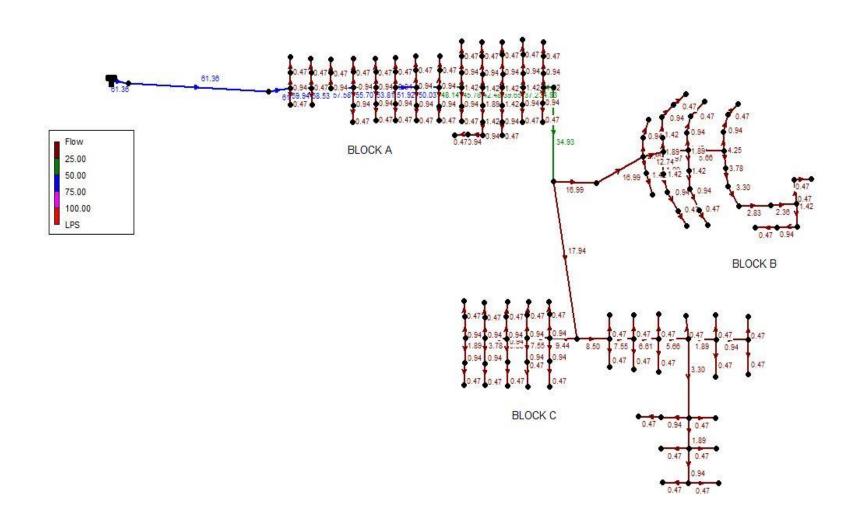


Figure 8 Epanet model showing irrigation system pressures for Kufandada irrigation network

Figure 9 Epanet model showing irrigation system flows in I/s for Kufandada irrigation network

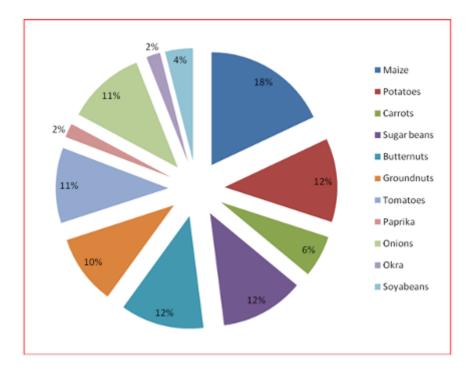


Day 1, 12:00 AM

### Proposed Agronomic Model

### **Cropping Patterns**

The selected cropping pattern for Kufandada Irrigation Scheme has been designed to increase agricultural production and the incomes of the poorest families, as well as strengthening organisation at grass-roots level. New high yielding and more profitable crops are proposed for the scheme as shown:



#### Figure 10 Proposed cropping programme

The selection of an intensive horticulture production of high value crops is predicated by the limited land size available as well as the need to maximise incomes among beneficiaries. Technical issues related to rotation and seasonality, diversity and the need for efficient utilization of irrigation water were also taken into consideration.

### Environmental protection

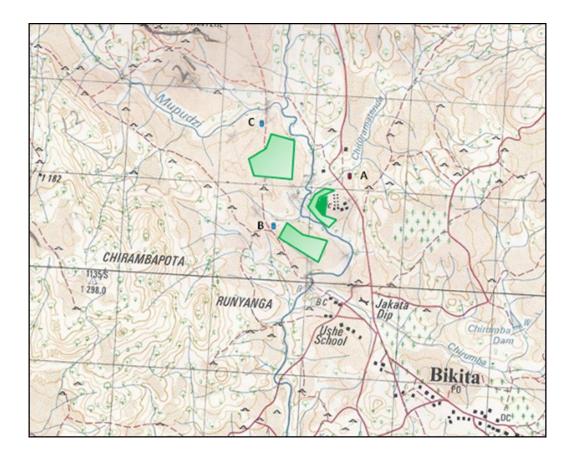
Extensive erosion is occurring on the left bank of Rozva River immediately downstream of Kufandada Dam. This erosion is slowly encroaching the area between the river and the main road. It is proposed to place gabion mats against the gulley walls to arrest the erosion

There is widespread stream bank and in-stream cultivation along the Rozva River and its tributaries. This has resulted in extensive water habitats destruction and siltation of water bodies. It is proposed to re-establish the statutory 30m buffer protection zones and plant grass and indigenous trees for protection in select areas.



### Water supply and sanitation

Options for the water supply were investigated, including connection to the ZINWA system and the provision of groundwater supplies. It is recommended that two new boreholes be drilled, as well as the rehabilitation of the broken down hand pump at the existing borehole; the location of the boreholes is shown below.



#### Figure 11 Location of proposed boreholes

### Sanitation

Access to proper sanitation facilities is still a challenge for many as they still practice open defecation. The ventilated-improved pit (VIP) latrine is recommended as the long term solution for sanitation in rural communities.

The proposed delivery mode for sanitation is for the project to supply selected building materials for 24 VIPs with the beneficiaries providing construction labour.



### Drawings

•

The following drawings have been prepared for the design of components of the scheme.

| Dra | awing Title  |  | Drawing No        |
|-----|--------------|--|-------------------|
| 1.  | General La   | yout (insert – locality Map)           | QW06/CE01         |
| 2.  | Plan and lo  | ongitudinal section of pumping mains   | QW06/CE02 SHT 1-5 |
| 3.  | Plan and lo  | ongitudinal section of suction mains   | QW06/CE03 SHT 1-9 |
| 4.  | Plan and lo  | ongitudinal section of suction mains   | QW06/CE04 SHT 1-5 |
| 5.  | Valve Char   | nber details                           | QW06/CE05         |
| 6.  | Pumping S    | tation and Weir Details                | QW06/CE06         |
| 7.  | River Cros   | sing Details                           | QW06/CE07         |
| 8.  | Anchor and   | Thrust Block Details                   | QW06/CE08         |
| 9.  | 2ml Galvar   | nised Steel Tank, Plan And Sections    | QW06/SE01         |
| 10. | Irrigation F | ield                                   |                   |
|     | 10.1.        | Layout of sprinkler system             |                   |
|     | 10.2.        | Erosion protection and drainage system |                   |
|     | 10.3.        | Blair Toilet                           |                   |



### **Cost Estimates**

A Bill of Quantities has been developed based on the abstraction of water from Rozva River, and the design and drawings for the proposed scheme described in the Report. The estimated cost for the implementation of Kufandada Irrigation Scheme is summarised below.

|   | SUMMARY                 |      |            |
|---|-------------------------|------|------------|
|   |                         |      |            |
| 1 | Pipeline                |      | 139,034.51 |
| 2 | 2.0 MI Reservoir        |      | 145,420.00 |
| 3 | Pump Station            |      | 74,990.00  |
| 4 | Infield Works           |      | 72,856.53  |
| 5 | Weir Construction       |      | 51,605.00  |
| 6 | Environmental           |      | 6,937.50   |
|   | Subtotal                |      | 490,843.54 |
|   |                         |      |            |
|   | Add CONTINGENCIES       | 0.10 | 49,084.35  |
|   | Add VAT 15%             | 0.15 | 73,626.53  |
|   |                         |      |            |
|   | TOTAL                   |      | 613,554.42 |
|   |                         |      |            |
|   | Management contractor   |      | 90,000.00  |
|   | Technical support costs |      | 12,000.00  |
|   | Direct labour costs     | 2%   | 9,203.32   |
|   |                         |      |            |
|   | GRAND TOTAL             |      | 724,757.74 |

A breakdown of costs is given in the priced Bill of Quantities in Appendix 3.

A comparison of bankability stage budget estimates against current estimates is given below:

### Kufandada Budget Review

| ltem | SUMMARY           | Feasibility Stage | Design<br>Stage | Difference | Comment  |
|------|-------------------|-------------------|-----------------|------------|--|
| 1    |                   |                   |                 |            | <ul><li>Pipe class for pumping main was increased to 16</li><li>additional steel sections</li></ul>  |
|      | PIPELINE          | 85,692.84         | 139,034.51      | 53,341.67  | <ul> <li>Pipe fittings were underestimated at the feasibility stage</li> </ul>   |
| 2    | 2.0 ML RESERVOIR  | 145,420.00        | 145,420.00      | 0.00       | -  |
| 3    |                   |                   |                 |            | <ul> <li>The 11kV overhead line was changed to 33kV because ZESA is no longer installing 11kV lines</li> <li>The transformer was upgraded from 200kVA to 500kVA</li> </ul> |
|      | PUMP STATION      | 56,000.00         | 74,990.00       | 18,990.00  | <ul> <li>Pump attendant's quarters was omitted at the<br/>feasibility stage</li> </ul>   |
| 4    | INFIELD WORKS     | 85,249.75         | 72,856.53       | -12,393.22 | Secondary infield pipes were reduced   |
| 5    | WEIR CONSTRUCTION | 51,605.00         | 51,605.00       | 0.00       | -  |
|      | ENVIRONMENTAL     | 6,937.50          | 6,937.50        | 0.00       | -  |

| SUBTOTAL                   | 430,905.09 | 490,843.54 | 59,938.45 | -                 |
|----------------------------|------------|------------|-----------|-------------------|
|                            |            |            |           |                   |
| Add CONTINGENCIES          | 43,090.51  | 49,084.35  | 5,993.84  | -                 |
| Add VAT 15%                | 64,635.76  | 73,626.53  | 8,990.77  | -                 |
|                            |            |            |           |                   |
| TOTAL                      | 538,631.36 | 613,554.42 | 74,923.06 | -                 |
|                            |            |            |           |                   |
| MANAGEMENT<br>CONTRACTOR   | 90,000.00  | 90,000.00  | 0.00      | -                 |
| TECHNICAL SUPPORT<br>COSTS | 12,000.00  | 12,000.00  | 0.00      | -                 |
| DIRECT LABOUR COSTS        | 8,079.47   | 9,203.32   | 1,123.85  | -                 |
|                            |            |            |           |                   |
| GRAND TOTAL                | 648,710.83 | 724,757.74 | 76,046.91 | • 10.4 % increase |

#### Appendices

#### Appendix 1: Proposed Weir Stability Calculations

| Project: Kufandada Imgation S  | DAM 2000 - C   | and the second se | and the second second second second                    | and the second | line has been                               |   |                                     |
|--|--|---|--|--|---|---|-------------------------------------|
| Dam: Kufandada Weir  | cheme  |   | performed by:  | Interconsult 2   | ampapwe                                     | _   | _                                   |
| Owner: Kufandada Imigation S   | cheme  |   |  | 11/02/2015 9   | :49   |   |                                     |
| Dam location: Bikita, Zimbebwe   |  |   | Units:   | Metric   |   |   |                                     |
| Conservation   |  |   |  | -  |   |   |                                     |
| L1= 4.000 m  | Concepts about a   |   |  | Properties   |   |   |                                     |
| L2= 0.000 m Mater  | ial Fc ft  | Cohesion  | friction<br>Angle                                      | Cohesion   | I friction<br>Angle                         |   | impressive<br>cohesion              |
| L3= 2.500 m nam  | Sector and the sector of the s |   | (deg)  | (kPa)  | (deg)                                       |   | Pa)                                 |
| L4= 1.000 m Base )   | oint 30000 0   | 0   | 55   | 0  | 45  |   | 0                                   |
| Elev. A= 899.000 m   | 0  |   |  |  |   |   |                                     |
| Elev. 8= 899.000 m<br>Elev. C= 901.000 m   |  |   | Lift Joint   |  |   |   |                                     |
| Elev. D= 900.000 m Join  |  | on Position x   | Elevation  | Position x   | Length                                      | Inc   | etha                                |
| Elev. E= 902.000 m id  | name (m)   | (m)   | (m)  | (m)  | (m)   |   | rM)                                 |
| Elev. F= 902.000 m Base  | e Base joint 899.00  | 0.000   | 000.698  | 4.000  | 4.000                                       |   | 333333                              |
| Ekev. G- 904.000 m   |  |   |  |  |   |   |                                     |
| Elev. H= 900.000 m   |  | ked Lift Join   |  |  |   |   |                                     |
| Elev. I = 900.000 m  |  | otream end  | 100000000000000000000000000000000000000                | ream end   |   |   |                                     |
| Concrete Volumetric Mass id  | Contraction of the second second   | ack length  |  | length   |   |   |                                     |
| p= 2400 kg/m <sup>3</sup> Base   | e Basejoint -  | (%)   | (m)  | (%)  |   |   |                                     |
| Bas  | - Dase Junt -  | 30  | 1 8 1  |  |   |   |                                     |
|  |  |   |  |  |   |   |                                     |
|  | ÷.,;   |   |  |  |   |   |                                     |
|  | a  |   | Reservoi   | 18   |   |   |                                     |
|  |  |   | Reservoi   |  | C   | Xewnstream si   | de                                  |
| Harrow Control Mass<br>p= 9.810 kg/m <sup>3</sup>  | Normal operating let   | vel:  |  | le   | C   | lownstream si   |                                     |
| H + C + D + D + D + D + D + D + D + D + D  | Normal operating lev<br>Flood lev  | vet:  | Upstream sid<br>904.000<br>906.500                     | n<br>m   | C   | 901.000<br>903.000  | m<br>m                              |
| L1<br>Water Volumetric Mass<br>p= 9.810 kg/m <sup>2</sup><br>Lcad= 0 kN<br>Thickness= 0.000 m  | Normal operating lev   | vet:  | Upstream sid<br>904.000                                | n<br>m   | C   | 901.000   | m<br>m                              |
| L1         0         1           Water Volumetric Mass         0         1           y=         9.810 kg/m²         1           Ice cover         1         1           Load=         0 kN         1           Prickmass=         0.000 m         1           Elevation=         900.000 m         1           1/2         7 kN/m²         65  | Normal operating lev<br>Flood lev  | vet:  | Upstream sid<br>904.000<br>906.500                     | n<br>m   | C   | 901.000<br>903.000  | m<br>m                              |
| L1<br>Water Volumetric Mass<br>g= 9.810 kg/m <sup>2</sup><br>Lcad# 0 kN<br>hickness* 0.000 m<br>Elevation# 900.000 m<br>1/* 7 kN/m <sup>2</sup><br>05 20 deg   | Normal operating lev<br>Flood lev<br>Crest overlopping press   | ure   | Upstream sid<br>904.000<br>906.500<br>100.00           | n<br>m<br>%  |   | 901.000<br>903.000  | m<br>m                              |
| La<br>Water Volumetric Mass<br>p= 9.810 kg/m <sup>2</sup><br>Load= 0 kN<br>hickness= 0.000 m<br>Elevation= 900.000 m<br>Silts<br>Elevation= 900.000 m<br>0= 20 deg<br>sumption= at rest  | Normal operating lev<br>Flood lev<br>Crest overlopping press   | ure   | Upstream sid<br>904.000<br>906.500<br>100.00           | le<br>m<br>m<br>%  | 969)  | 901.000<br>903.000  | m<br>m                              |
| Li<br>Water Volumetric Mass<br>p= 9.810 kg/m <sup>3</sup><br>Lcc cover<br>Load= 0 kN<br>Dickness= 0.000 m<br>Elevation= 904.000 m<br>1/* 7 kN/m <sup>2</sup><br>c= 20 deg<br>sumption= at rest<br>Uplift pressures: Uplift pressu  | Normal operating lea<br>Flood lea<br>Crest overlopping press<br>res are considered as an e<br>Craci  | ure<br>ure  | Upstream sid<br>904.000<br>906.500<br>100.00           | In<br>m<br>%<br>Mactive stress<br>Fensile stress   | ees)  | 901.000<br>903.000<br>50.00                                   | m<br>**                             |
| La<br>Water Volumetric Mass<br>p= 9.810 kg/m <sup>2</sup><br>Load= 0 kN<br>Pickness= 0.000 m<br>Elevation= 900.000 m<br>Silts<br>Elevation= 900.000 m<br>0= 20 deg<br>sumption= at rest  | Normal operating lea<br>Flood lea<br>Crest overlopping press<br>res are considered as an e<br>Craci  | vet:<br>ure<br>external load (in<br>king options  | Upstream sid<br>904.000<br>906.500<br>100.00           | In<br>m<br>%<br>Mactive stress<br>Censile stress<br>Usual  | 969)  | 901.000<br>903.000  | m<br>m                              |
| Li       Image: Construction of the second sec | Normal operating lea<br>Flood lea<br>Crest overlopping press<br>res are considered as an e<br>Craci  | vet:<br>ure<br>external load (lin<br>king options   | Upstream sid<br>904.000<br>906.500<br>100.00           | Ite<br>m<br>%<br>%<br>//fective stress<br>Usual<br>ft / 3.000  | ees)<br>gth<br>Flood                        | 901.000<br>903.000<br>50.00<br>Seismic                        | m<br>%<br>%                         |
| Li       Use of the second secon | Normal operating lea<br>Flood lea<br>Crest overlopping press<br>res are considered as an e<br>Craci  | ett<br>ure<br>external load (lin<br>king options<br>Crack   | Upstream sid<br>904.000<br>906.500<br>100.00<br>100.00 | Ite<br>m<br>%<br>%<br>//fective stress<br>Usual<br>ft / 3.000  | ess)<br>Flood<br>ft / 3.000<br>ft / 10.000, | 901.000<br>903.000<br>50.00<br>50.00<br>Seismic<br>ft / 3.000 | m<br>%<br>%<br>Post-sets<br>ft/3.00 |

| CADAM 200                            | 00 - Result report                         |  |
|--------------------------------------|--|--|
| Project: Kufandada Irrigation Scheme | Project engineer: Interconsult Zimbabwe    |  |
| Dam: Kufandada Weir                  | <ul> <li>Analysis performed by:</li> </ul> |  |
| Owner: Kufandada Irrigation Scheme   | Date: 11 February 15                       |  |
| Dam location: Bikita, Zimbabwe       | Units: Metric                              |  |

|                          | Usual                 | Flood | Seismic #1 | Seismic #2 | Post-seismic |
|--------------------------|-----------------------|-------|------------|------------|--------------|
| Self-weight              | 1.000                 |       |            |            |              |
| Hydrostatic (upstream)   | 1.000                 |       |            |            |              |
| Hydrostatic (downstream) | 1.000                 |       |            |            |              |
| Uplift pressures         | 1.000                 |       |            |            |              |
| Silts                    |                       |       |            |            |              |
| ce                       |                       |       |            |            |              |
| Post-tensioning          | and the second second |       |            |            |              |
| Applied forces           |                       |       |            |            |              |
| Seismic (horizontal)     |                       |       |            |            |              |
| Seismic (vertical)       |                       |       |            |            |              |

|    |                           |     | 030        | JAL  | CO M        | DINAI    | ION (S                                  | IKES    | S ANA       | LISI     | 31      | and the second second |            |
|----|---------------------------|-----|------------|------|-------------|----------|---|---------|-------------|----------|---------|-----------------------|------------|
| 1  | loint                     |     | Crac       | king |             |          | Stresses                                |         |             |          |         |                       |            |
|    | Joint Upstream Downstream |     |            |      |             | Normal   | Normal stresses alowable stresses Shear |         |             |          |         | Shear                 |            |
| ID | Upstream elevation        |     | ack<br>gth | 100  | ack<br>Igth | Upstream | Downstream                              | tension | Compression | Upstream | Maximum | Maximum at<br>I-axis  | Downstream |
|    | (m)                       | (%) | (m)        | (%)  | (m)         | (kPa)    | (kPa)                                   | (kPa)   | (kPa)       | (kPa)    | (kPa)   | (% of joint)          | (kPa)      |
| 1  | Base                      | 100 | 1222       | 1.1  |             | -13.098  | -84.879                                 | 0.000   | -9990.000   | 0.000    | 38.627  | 50.000                | 0.000      |

|    |                       | US    | UAL      | COM           | BINA          | TION      | (STAB  | LITY  | ANAL   | YSIS)        |        |                     |
|----|-----------------------|-------|----------|---------------|---------------|-----------|--------|-------|--------|--------------|--------|---------------------|
|    | loint                 |       | 5        | Safety fac    | tors          |           |        | Resul | tants  |              | Uplift | Rock                |
| 9  | ome                   | Şli   | ding     | Overt         | urning        | Uplifting | Normal | Shear | Moment | Position     | Final  | Passive             |
| ID | Upstream<br>elevation | Peak  | Residual | Toward<br>U/S | Toward<br>D/S |           |        |       |        |              | Force  | wedge<br>resistance |
|    | (m)                   |       |          |               |               |           | (kN)   | (kN)  | (kN-m) | (% of joint) | (kN)   | (kN)                |
| 1  | Base                  | 2.717 | 1.902    | 2.962         | 1.571         | 2.427     | -196.0 | 103.0 | 95.7   | 62.211       | 137.3  | 0.000               |

|    |                       |      | FLO                 | DOD  | COM         | BINAT                              | ION (S     | TRES    | SANA        | LYSI     | S)       |                      |            |
|----|-----------------------|------|---------------------|------|-------------|------------------------------------|------------|---------|-------------|----------|----------|----------------------|------------|
|    | loint                 |      | Crac                | king |             | Stresses                           |            |         |             |          |          |                      |            |
|    | ioint.                | Upst | Upstream Downstream |      |             | Normal stresses, alowable stresses |            |         | Shear       |          |          |                      |            |
| ID | Upstream<br>elevation |      | ack<br>agth         |      | ack<br>ngth | Upstream                           | Downstream | tension | Compression | Upstream | Maximum  | Maximum at<br>I-axis | Downstream |
|    | (m)                   | (%)  | (m)                 | (%)  | (m)         | (kPa)                              | (kPa)      | (kPa)   | (kPa)       | (kPa)    | (kPa)    | (% of joint)         | (kPa)      |
| 1  | Base                  |      |                     |      |             | 0.000                              | 0.000      | 0.000   | -15000.000  |          | 201 . 22 | - 10                 | 100 100    |

|       |                       | FLO            | OOD      | COM           | BINA          | TION      | (STAB  | LITY         | ANAL   | YSIS)        |       |                     |
|-------|-----------------------|----------------|----------|---------------|---------------|-----------|--------|--------------|--------|--------------|-------|---------------------|
|       | loint                 | Safety factors |          |               |               |           | Resul  | tants        |        | Uplift       | Rock  |                     |
| Joint |                       | Sli            | ding     | Overt         | urning        | Uplifting | Normal | Normal Shear |        | Position     | Final | Passive             |
| D     | Upstream<br>elevation | Peak           | Residual | Toward<br>U/S | Toward<br>D/S |           |        |              |        |              | Force | wedge<br>resistance |
|       | (m)                   |                |          |               | -             |           | (kN)   | (kN)         | (kN-m) | (% of joint) | (kN)  | {kN}                |
| 1     | Base                  | > 100          | > 100    | > 100         | > 100         | > 100     | 0.0    | 0.0          | 0.0    | 50.000       | 225.6 | 0.000               |
|       | Required:             | 2,000          | 1,300    | 1,100         | 1.100         | 1.100     |        |              |        |              |       |                     |

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## Appendix 2: Letter of undertaking to enter into a memorandum of Agreement with ZINWA





#### Appendix 3: Bill of Quantities

| Item    | Description                         | Qty   | Unit | Rate     | Cost      |
|---------|-------------------------------------|-------|------|----------|-----------|
| 1       | PIPELINE                            |       |      |          |           |
|         |                                     |       |      |          |           |
| 1.3     | Pipe Laying                         |       |      |          |           |
| 1.3.1   | Supply MPVC pumping mains           |       |      |          |           |
|         | a) 200 mm dia Class 16              | 840   | m    | 39.22    | 32,944.80 |
|         |                                     |       |      |          |           |
| 1.3.2   | Supply MPVC gravity mains           |       |      |          |           |
|         | a) 250 mm dia Class 6               | 482   | m    | 26.98    | 13,004.36 |
|         | b)200mm dia Class 6                 | 601.5 | m    | 17.65    | 10,616.48 |
|         | c)160mm dia Class 6                 | 773   | m    | 11.52    | 8,904.96  |
|         |                                     |       |      |          |           |
| 1.3.3   | Supply Steel gravity mains          |       |      |          |           |
|         | a) 160 mm dia PN 160                | 105   | m    | 80.75    | 8,478.75  |
|         |                                     |       |      |          |           |
| 1.3.3   | Supply and install fittings pumping |       |      |          |           |
|         | mains                               |       |      |          |           |
| 1.3.3.1 | mPVC (Class 6) Bends                |       |      |          |           |
|         | a) 200 x 45°                        | 0     | No.  | 71.04    | 0.00      |
|         | b) 200 x 22,5°                      | 2     | No.  | 71.04    | 142.08    |
|         | c) 200 x 11,25°                     | 5     | No.  | 71.04    | 355.20    |
|         |                                     |       |      |          |           |
| 1.3.3.2 | GI Bends                            |       |      |          |           |
|         | a) 200 x 45°                        | 2     | No.  | 700.00   | 1,400.00  |
|         | b) 200 x 22,5°                      | 4     | No.  | 700.00   | 2,800.00  |
|         | c) 200 x 11,25°                     | 1     | No.  | 700.00   | 700.00    |
|         |                                     |       |      |          |           |
| 1.3.3.3 | CI reducers                         |       |      |          |           |
|         | a) 250/200                          | 0     | No.  |          |           |
|         |                                     |       |      |          |           |
| 1.3.3.4 | PVC Tees                            |       |      |          |           |
|         | 200 dia equal tee                   | 0     | No.  | 133.75   | 0.00      |
|         |                                     |       |      |          |           |
| 1.3.3.5 | CI Gate valves                      |       |      |          |           |
|         | a) 250 dia                          | 2     | No.  | 2,500.00 | 5,000.00  |
|         | b) 200 dia                          | 0     | No.  | 2,500.00 | 0.00      |
|         |                                     |       |      |          |           |
| 1.3.3.6 | Air Valves                          |       |      |          |           |



|         | a) 250 dia                                       | 0  | No.  | 1,200.00 | 0.00     |
|---------|--|----|------|----------|----------|
|         | b) 200 dia                                       | 2  | No.  | 1,200.00 | 2,400.00 |
|         | 5) 200 014                                       | ۷  | NO.  | 1,200.00 | 2,400.00 |
| 1.3.3.7 | Scour Valves                                     |    |      |          |          |
| 1.0.0.7 | a) 250 dia                                       | 0  | No.  | 1,200.00 | 0.00     |
|         | b) 200 dia                                       | 2  | No.  | 1,200.00 | 2,400.00 |
|         | 5) 200 01a                                       | ۷  | 110. | 1,200.00 | 2,400.00 |
| 1.3.4   | Allow for bulk water meter to suit 200mm         | 1  | No   | 4,000.00 | 4,000.00 |
|         | MPVC pipe  |    |      |          |          |
|         |  |    |      |          |          |
|         |  |    |      |          |          |
| 2.4     | Supply and install fittings for gravity<br>mains |    |      |          |          |
|         |  |    |      |          |          |
| 2.4.1   | mPVC (Class 6) Bends                             |    |      |          |          |
|         | b) 200 x 45°                                     | 9  | No.  | 71.04    | 639.36   |
|         | c) 200 x 22,5°                                   | 7  | No.  | 71.04    | 497.28   |
|         | d) 200 x 11,25°                                  | 7  | No.  | 71.04    | 497.28   |
|         | e) 250 x 90°                                     | 1  | No.  | 124.48   | 124.48   |
|         | f) 250 x 45°                                     | 2  | No.  | 96.31    | 192.62   |
|         | g) 250 x 22,5°                                   | 10 | No.  | 96.31    | 963.10   |
|         | h) 250 x 11,25°                                  | 21 | No.  | 96.31    | 2,022.51 |
|         |  |    |      |          |          |
| 2.4.2   | GI Bends   |    |      |          |          |
|         | b) 200 x 45°                                     | 2  | No.  | 750.00   | 1,500.00 |
|         | c) 200 x 22,5°                                   | 4  | No.  | 750.00   | 3,000.00 |
|         | d) 200 x 11,25°                                  | 1  | No.  | 750.00   | 750.00   |
|         |  |    |      |          |          |
| 2.4.4   | CI reducers                                      |    |      |          |          |
|         | a) 250/200                                       | 1  | No.  | 850.00   | 850.00   |
|         |  |    |      |          |          |
| 2.4.5   | PVC Tees   |    |      |          |          |
|         | 200 dia equal tee                                | 1  | No.  | 133.75   | 133.75   |
| 2.4.6   | CI Gate valves                                   |    |      |          |          |
|         | a) 250 dia                                       | 2  | No.  | 2,500.00 | 5,000.00 |
|         | b) 200 dia                                       | 3  | No.  | 2,500.00 | 7,500.00 |
|         |  |    | 110. | 2,000.00 | .,000.00 |
| 2.4.7   | Air Valves                                       |    |      |          |          |
|         | a) 250 dia                                       | 2  | No.  | 1,200.00 | 2,400.00 |



|          | h) 200 dia                             | 2   | Na             | 1 200 00  | 2 000 00   |
|----------|--|-----|----------------|-----------|------------|
|          | b) 200 dia                             | 3   | No.            | 1,200.00  | 3,600.00   |
|          |  |     |                |           |            |
| 2.4.8    | Scour Valves                           |     |                |           |            |
|          | a) 250 dia                             | 2   | No.            | 1,200.00  | 2,400.00   |
|          | b) 200 dia                             | 4   | No.            | 1,200.00  | 4,800.00   |
|          |  |     |                |           |            |
| 1.4      | Sundries                               |     |                |           |            |
|          |  |     |                |           |            |
| 1.4.1    | Precast Concrete Valve Boxes 700mm x   | 5   | No             | 510.00    | 2,550.00   |
|          | 400mm C/W concrete lids                |     | _              |           | ,          |
|          |  |     |                |           |            |
| 1.4.2    | a) Valve Marker Posts                  | 5   | No             | 97.50     | 487.50     |
| 1.4.2    |  | 5   |                | 97.50     | 407.50     |
| 1.4.3    |  | 2   | m <sup>3</sup> | 165.00    | 220.00     |
| 1.4.3    | Allow for concrete thrust blocks at    | Z   | (II)           | 165.00    | 330.00     |
|          | every change on pipe direction Grade   |     |                |           |            |
|          | <u>15</u>                              |     |                |           |            |
|          |  |     | 2              |           |            |
| 1.4.4    | Allow for concrete encasing where      | 10  | m <sup>3</sup> | 200.00    | 2,000.00   |
|          | directed                               |     |                |           |            |
|          |  |     |                |           |            |
| 1.4.5    | Allow for concrete anchor blocks on    | 10  | m <sup>3</sup> | 165.00    | 1,650.00   |
|          | steep grades                           |     |                |           |            |
|          |  |     |                |           |            |
| 1.4.6    | Allow for connection to reservoir      | 1   | P.Sum          | 2,000.00  | 2,000.00   |
|          |  |     |                |           |            |
|          | TOTAL FOR PIPELINE                     |     |                |           | 139,034.51 |
|          |  |     |                |           | 133,034.31 |
|          | (carried to summary)                   |     |                |           |            |
|          |  |     |                |           |            |
| 0        |  |     |                |           |            |
| 2        | 2.0 ML RESERVOIR                       |     |                |           |            |
|          |  |     |                | D 4 7 7   |            |
| ITEM     | DESCRIPTION                            | QTY | UNIT           | RATE      | AMOUNT     |
| <u> </u> |  |     |                |           |            |
| 2.1      | Galvanized Water Storage Tank          |     |                |           |            |
|          | Installation                           |     |                |           |            |
|          |  |     |                |           |            |
| 2.1.1    | Supply and fix 1,000L galvanised steel | 2   | No             | 55,000.00 | 110,000.00 |
|          | tank                                   |     |                |           |            |
|          |  |     |                |           |            |



| 2.1.2 | Earthworks (leveling and sub base and hardcore compaction) |       | Sum  | 5,000.00  | 5,000.00   |
|-------|--|-------|------|-----------|------------|
|       |  |       |      |           |            |
| 2.2   | Construction of floor                                      |       |      |           |            |
|       |  |       |      |           |            |
| 2.2.1 | Concrete Class 15/20 in sub-foundation blinding.           | 60    | m3   | 180.00    | 10,800.00  |
|       |  |       |      |           |            |
| 2.3   | High tensile round deformed                                |       |      |           |            |
|       | reinforcement. Supply, bend, place                         |       |      |           |            |
|       | and fix.   |       |      |           |            |
| 2.3.1 | 12mm dia. and smaller.                                     | 10900 | ka   | 1 50      | 16 200 00  |
| 2.3.1 |  | 10800 | kg   | 1.50      | 16,200.00  |
| 2.4   | Formwork   |       |      |           |            |
| 2.7   |  |       |      |           |            |
| 2.4.1 | Apply 1:3 cement mortar screed 12mm                        | 285   | m2   | 12.00     | 3,420.00   |
|       | thick to top of no fines concrete lower                    |       |      |           | -,         |
|       | floor slab, steel trowel finish.                           |       |      |           |            |
|       |  |       |      |           |            |
|       | TOTAL FOR RESERVOIR  |       |      |           | 145,420.00 |
|       | (carried to summary)                                       |       |      |           |            |
|       |  |       |      |           |            |
| 3     | PUMP STATION   |       |      |           |            |
|       |  |       |      |           |            |
| ITEM  | DESCRIPTION  | QTY   | UNIT | RATE      | AMOUNT     |
|       |  |       |      |           |            |
| 3.1   | 33 kV line construction                                    | 0.5   | km   | 10,000.00 | 5,000.00   |
|       |  |       |      |           |            |
| 3.2   | Supply and install 500 Kva, 33kV/400V                      | 1     | Sum  | 35,000.00 | 15,000.00  |
|       | transformer  |       |      |           |            |
| 3.3   | Supply and install pump set                                | 2     |      | 10 500 00 | 21 000 00  |
| 3.3   | Supply and install pump set                                | ۷     | Sum  | 10,500.00 | 21,000.00  |
| 3.4   | Construct Pump house and ancillaries                       | 1     | Sum  | 15,000.00 | 15,000.00  |
| 5.4   | construct any nouse and anomalies                          |       | Cum  | 10,000.00 | 10,000.00  |
| 3.5   | Construct Pump Attendant's Quarters                        | 1     | Sum  | 12,000.00 | 12,000.00  |
|       |  |       |      | ,         | ,          |
|       | TOTAL FOR PUMP STATION                                     |       |      |           | 68,000.00  |
|       | (corrigate our more a)                                     |       |      |           |            |
|       | (carried to summary)                                       |       |      |           |            |

| 4        | INFIELD WORKS                          |       |      |        |          |
|----------|--|-------|------|--------|----------|
|          |  |       |      |        |          |
| ITEM     | DESCRIPTION                            | QTY   | UNIT | RATE   | AMOUNT   |
|          |  |       |      |        |          |
| 4.1      | Land preparation and levelling         | 15    | На   | 600    | 9,000.00 |
| 4.2      | Fencing the irrigation scheme          | 1,923 | m    | 3.25   | 6,249.75 |
|          |  |       |      |        |          |
| 4.3      | Sprinkler irrigation system            |       |      |        |          |
| 4.3.1    | Supply and Install infield Sprinkler   |       |      |        |          |
|          | system                                 |       |      |        |          |
|          |  |       |      |        |          |
| 4.3.1.1  | 5mm brass Sprinklers 3 bars, 1.7m3/hr, | 120   |      | 28.00  | 3,360.00 |
|          | 7.87mm/hr                              |       |      |        |          |
| 4.3.1.2  | 20mm brass garden tape                 | 120   |      | 22.60  | 2,712.00 |
| 4.3.1.3  | 1m x 20mm GI riser pipes               | 120   |      | 6.55   | 786.00   |
| 4.3.1.4  | 20mm elbows                            | 240   |      | 1.25   | 300.00   |
| 4.3.1.5  | 1m tripod stand complete with 1m GI    | 120   |      | 29.84  | 3,580.80 |
|          | riser pipe                             |       |      |        |          |
| 4.3.1.6  | 32m x 20mm reinforced garden hose      | 120   |      | 62.40  | 7,488.00 |
| 4.3.1.7  | 20mm GI sockets                        | 240   |      | 0.85   | 204.00   |
| 4.3.1.8  | 20mm swage nipples                     | 240   |      | 1.65   | 396.00   |
| 4.3.1.9  | 20-25 Dupli clips                      | 240   |      | 0.75   | 180.00   |
| 4.3.1.10 | Thread tape rolls                      | 500   |      | 0.20   | 100.00   |
| 4.3.1.11 | 40mm Brass gate valves                 | 20    |      | 42.00  | 840.00   |
| 4.3.1.12 | 50mm Brass gate valves                 | 15    |      | 56.00  | 840.00   |
| 4.3.1.13 | 63mm Brass gate valves                 | 6     |      | 60.00  | 360.00   |
| 4.3.1.14 | 75mm Brass gate valve                  | 2     |      | 84.50  | 169.00   |
| 4.3.1.15 | 90mm Brass gate valve                  | 2     |      | 105.00 | 210.00   |
| 4.3.1.16 | 110mm Cast iron gate valve             | 2     |      | 149.80 | 299.60   |
| 4.3.1.17 | 500 ml Solvent cement                  | 4     |      | 17.82  | 71.28    |
|          |  |       |      |        |          |
| 4.3.2    | Supply HDPE                            |       |      |        |          |
|          | a) 40mm Class 6                        | 4,130 | m    | 1.30   | 5,368.90 |
|          | b) 50mm Class 6                        | 3,423 | m    | 1.30   | 4,449.90 |
|          |  |       |      |        |          |
| 4.3.3    | Supply MPVC pipework                   |       |      |        |          |
|          | a) 40mm Class 6                        | 201   | m    | 1.23   | 247.23   |
|          | b) 50mm Class 6                        | 214   | m    | 1.69   | 362.20   |
|          | c) 63mm Class 6                        | 177   | m    | 2.14   | 378.78   |

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|       | d) 75mm Class 6                          | 252    | m    | 2.58   | 650.16    |
|-------|--|--------|------|--------|-----------|
|       | f) 110mm Class 6                         | 295    | m    | 5.21   | 1,535.70  |
|       | h) 160mm Class 6                         | 872    | m    | 11.52  | 10,048.67 |
|       | i) 200mm Class 6                         | 577    | m    | 17.65  | 10,178.93 |
|       |  | 011    |      | 11.00  | 10,110.00 |
| 4.3.4 | MPVC bends to suite MPVC pipes           |        |      |        |           |
|       | a) 200 mm 90 deg                         | 1      | No   | 83.58  | 83.58     |
|       | b) 160 mm 45 deg                         | 2      | No   | 45.76  | 91.52     |
|       | c) 160 mm 22.5 deg                       | 4      | No   | 45.76  | 183.04    |
|       | d) 160 mm 11.25 deg                      | 2      | No   | 45.76  |           |
|       | d) 110 mm 22.5 deg                       | 2      | No   | 17.70  | 35.40     |
|       | , , , , , , , , , , , , , , , , , , ,    |        |      |        |           |
| 4.3.5 | Tees                                     |        |      |        |           |
|       | a) 200/50 unequal Tee                    | 10     | No   | 128.73 | 1,287.30  |
|       | b) 200/40 unequal Tee                    | 3      | No   | 128.73 | 386.19    |
|       | d) 160/75 unequal Tee                    | 1      | No   | 72.60  | 72.60     |
|       | e) 110/40 unequal Tee                    | 1      | No   | 27.36  | 27.36     |
|       | f) 75/40 unequal Tee                     | 5      | No   | 18.91  | 94.55     |
|       | g) 75/63 unequal Tee                     | 1      | No   | 57.91  | 57.91     |
|       | h) 50/40 unequal Tee                     | 5      | No   | 18.91  | 94.55     |
|       | i) 40 equal Tee                          | 4      | No   | 18.91  | 75.64     |
|       |  |        |      |        |           |
|       | TOTAL FOR INFIELD WORKS                  |        |      |        | 72,856.53 |
|       | (carried to summary)                     |        |      |        |           |
|       |  |        |      |        |           |
| 5     | WEIR CONSTRUCTION                        |        |      |        |           |
|       |  |        |      |        |           |
| ITEM  | DESCRIPTION                              | QTY    | UNIT | RATE   | AMOUNT    |
| 5.1   | Clearing of site, excavations (including | 700    | m3   | 5      | 3,500.00  |
|       | rock blasting) for weir of length 74m    |        |      |        |           |
| 5.2   | Weir construction: 74m of 1,5m high      | 172.42 | m3   | 250    | 43,105.00 |
|       | masonry including foundations            |        |      |        |           |
| 5.3   | Clearing area, diversion                 | 1      | Sum  | 5000   | 5,000.00  |
|       | works/cofferdam construction,            |        |      |        |           |
|       | excavations for pump house sump          |        |      |        |           |
|       | TOTAL FOR WEIR CONSTRUCTION              |        |      |        | 51,605.00 |
|       | (carried to summary)                     |        |      |        |           |
|       |  |        |      |        |           |
| 6     | ENVIRONMENTAL                            |        |      |        |           |
|       |  |        |      |        |           |



| ITEM | DESCRIPTION                              | QTY  | UNIT  | RATE | AMOUNT     |
|------|--|------|-------|------|------------|
|      |  |      |       |      |            |
| 6.1  | Allow for environmental protection works | 1    | Sum   |      | 6,000.00   |
|      | by use of gabions and buffles            |      |       |      |            |
| 6.2  | Tree seedlings and planting              | 1250 | plant | 0.75 | 937.50     |
|      |  |      |       |      |            |
|      | TOTAL FOR ENVIRONMENTAL                  |      |       |      | 6,937.50   |
|      | (carried to summary)                     |      |       |      |            |
|      |  |      |       |      |            |
|      |  |      |       |      |            |
|      | SUMMARY                                  |      |       |      |            |
|      |  |      |       |      |            |
| 1    | PIPELINE                                 |      |       |      | 139,034.51 |
| 2    | 2.0 ML RESERVOIR                         |      |       |      | 145,420.00 |
| 3    | PUMP STATION                             |      |       |      | 68,000.00  |
| 4    | INFIELD WORKS                            |      |       |      | 72,856.53  |
| 5    | WEIR CONSTRUCTION                        |      |       |      | 51,605.00  |
| 6    | ENVIRONMENTAL                            |      |       |      | 6,937.50   |
|      | SUBTOTAL                                 |      |       |      | 483,853.54 |
|      |  |      |       |      |            |
|      | Add CONTINGENCIES                        |      |       | 0.10 | 48,385.35  |
|      | Add VAT 15%                              |      |       | 0.15 | 72,578.03  |
|      |  |      |       |      |            |
|      | TOTAL                                    |      |       |      | 604,816.92 |
|      |  |      |       |      |            |
|      | MANAGEMENT CONTRACTOR                    |      |       |      | 90,000.00  |
|      | TECHNICAL SUPPORT COSTS                  |      |       |      | 12,000.00  |
|      | DIRECT LABOUR COSTS                      |      |       | 2%   | 9,072.25   |
|      |  |      |       |      |            |
|      | GRAND TOTAL                              |      |       |      | 715,889.18 |

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